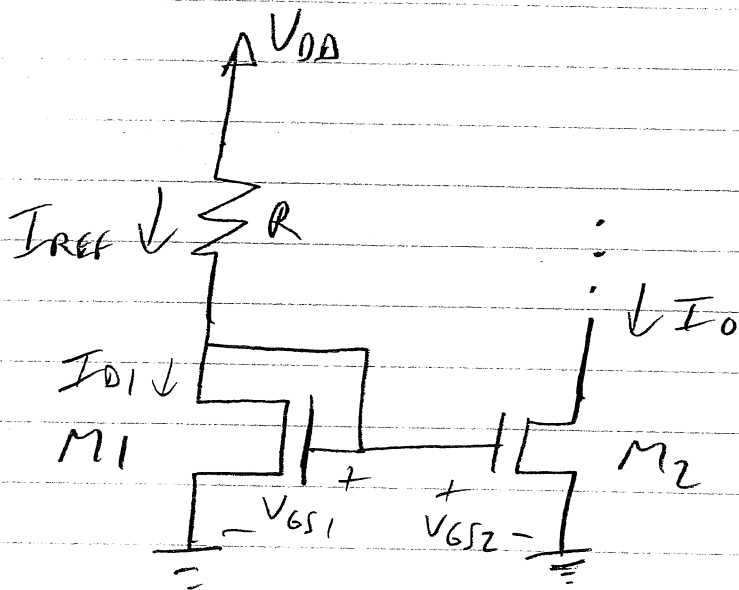


# CURRENT MIRRORS

CM1



ASSUME

$$\mu_N = \mu_{N1} = \mu_{N2}$$

$$C_{ox} = C_{ox1} = C_{ox2}$$

$$V_{th} = V_{th1} = V_{th2}$$

FOR M1

$V_{DS} = V_{GS} \Rightarrow$  ACTIVE OR CUTOFF  
NOT TRIODE

(SINCE  $V_{DS} < V_{GS} - V_{th}$  FOR TRIODE)

IF  $I_{REF} \neq 0 \Rightarrow$  ACTIVE

$$I_{D1} = \frac{\mu_N C_{ox}}{2} \left(\frac{W}{L}\right)_1 V_{OV1}^2$$

$$V_{OV1} = V_{GS1} - V_{th1}$$

①

$$I_{D1} = I_{REF} = \frac{V_{DD} - V_{GS1}}{R}$$

FOR M2

$$I_0 = I_{D2} = \frac{\mu_N C_{ox}}{2} \left(\frac{W}{L}\right)_2 V_{OV2}^2$$

②

CM2

COMBINE (1) & (2)

$$\frac{I_{D2}}{I_{D1}} = \frac{(W/L)_2}{(W/L)_1} \quad \text{CURRENT MIRROR}$$

$$\text{So } \frac{I_o}{I_{REF}} = \frac{(W/L)_2}{(W/L)_1}$$

VALID AS LONG AS M2 REMAINS ACTIVE

$$\Rightarrow V_o \geq V_{OV2} \quad \text{SINCE } V_{DS2} = V_o$$

EX GIVEN  $I_{REF} = 40 \mu A$   $\mu_n C_{ox} = 120 \mu A/V^2$

- FIND  $W_2$  SO THAT  $I_{OUT} = 20 \mu A$   $V_{th} = 0.3 V$
- FIND OUTPUT IMPEDANCE OF CURRENT SOURCE  $L = 0.2 \mu m$
- FIND LOWEST POSSIBLE  $V_o$  (KEEPING M2 ACTIVE)  $V_A' = 20 V/\mu m$
- FIND  $\Delta I_{OUT}$  IF  $\Delta V_o = +1 V$   $W_1 = 2 \mu m$

(CM3)

$$40 \mu A = I_{O1} = \frac{\mu_n C_{ox}}{2} \left( \frac{W_1}{L} \right) (V_{OV1})^2$$

$$40 \mu A = \frac{(120 \text{ e-6})}{2} \left( \frac{2}{0.2} \right) (V_{OV1})^2$$

$$V_{OV1} = \underline{\underline{0.258}} \quad \text{OR} \quad -0.258$$

X NOT POSSIBLE

$$\frac{I_{OUT}}{I_{REF}} = \frac{\left( \frac{W_2}{L} \right)}{\left( \frac{W_1}{L} \right)} = \frac{W_2}{W_1}$$

$$W_2 = \frac{I_{OUT}}{I_{REF}} W_1 = \frac{20 \mu A}{40 \mu A} (2 \mu m)$$

$$W_2 = \underline{\underline{1 \mu m}}$$

$$r_{O2} = \frac{V_A}{I_{O2}} = \frac{V_A' L}{I_{O2}} = \frac{(20)(0.2)}{20 \mu A}$$

$$r_{O2} = \underline{\underline{200 \text{ k}\Omega}}$$

SINCE  $V_{GS2} = V_{GS1}$  &  $V_{th1} = V_{th2}$

$$V_{OV2} = V_{GS2} - V_{th2} = V_{GS1} - V_{th1} = V_{OV1}$$

$$\text{MIN } V_0 = V_{OV2} = 0.258 \text{ V} \approx 0.25 \text{ V}$$

(CM4)

$$\Delta I_{out} = \frac{\Delta V_o}{r_{o2}} = \frac{1V}{200k} = 5 \mu A$$

SO A 1V CHANGE RESULTS IN

A 25% CHANGE IN  $I_{out}$

- AT WHAT WHAT  $V_o$  DOES  $I_{out} = 20 \mu A$ ?

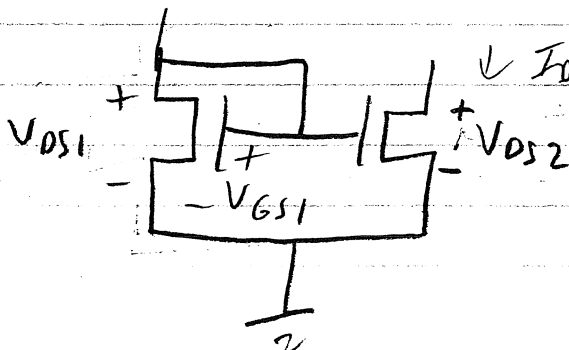
RECALL 
$$I_D = \left(\frac{\mu_n C_{ox}}{2}\right) \left(\frac{W}{L}\right) (V_{GS} - V_{th})^2 (1 + \lambda V_{DS})$$

SO  $I_D$  DEPENDS ON  $V_{GS}$  &  $V_{DS}$  &  $V_{th}$

IF  $V_{GS2} = V_{GS1}$  ,  $V_{th2} = V_{th1}$   
 $V_{DS2} = V_{DS1}$  ,  $L_2 = L_1$  (TO KEEP  $\lambda_2 = \lambda_1$ )

THEN  $I_{D2} = \frac{W_2}{W_1} I_{D1}$

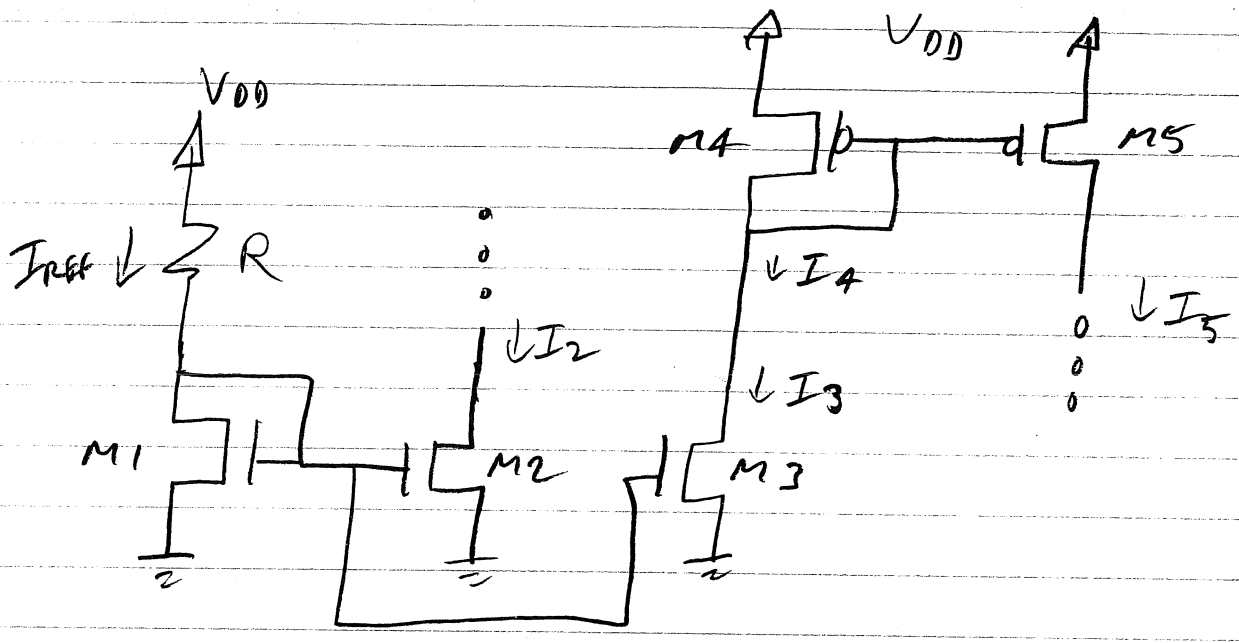
SO  $I_{D2} = 20 \mu A$  FOR  $V_o = V_{GS1} = V_{ov} + V_{th}$   
 $= 0.558$



$I_{D2} = I_{out}$

ENSURE  $L_2 = L_1$

SENDING BIAS CURRENTS AROUND A CHIP



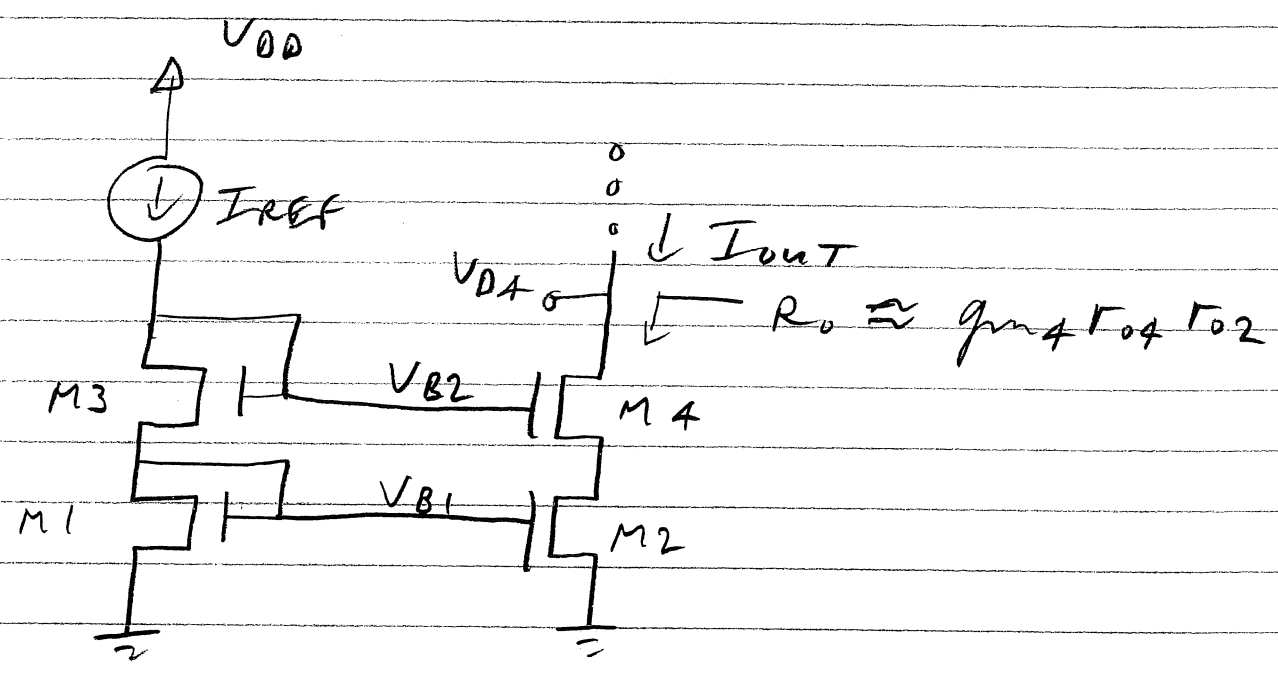
$$I_2 = \frac{(W/L)_2}{(W/L)_1} I_{REF}$$

$$I_3 = \frac{(W/L)_3}{(W/L)_1} I_{REF} = I_4$$

$$I_5 = \frac{(W/L)_5}{(W/L)_4} I_4 = \frac{(W/L)_3}{(W/L)_1} \frac{(W/L)_5}{(W/L)_4} I_{REF}$$

CASCODE MOS MIRROR

TO IMPROVE OUTPUT IMPEDANCE OF CURRENT MIRROR => CASCODE



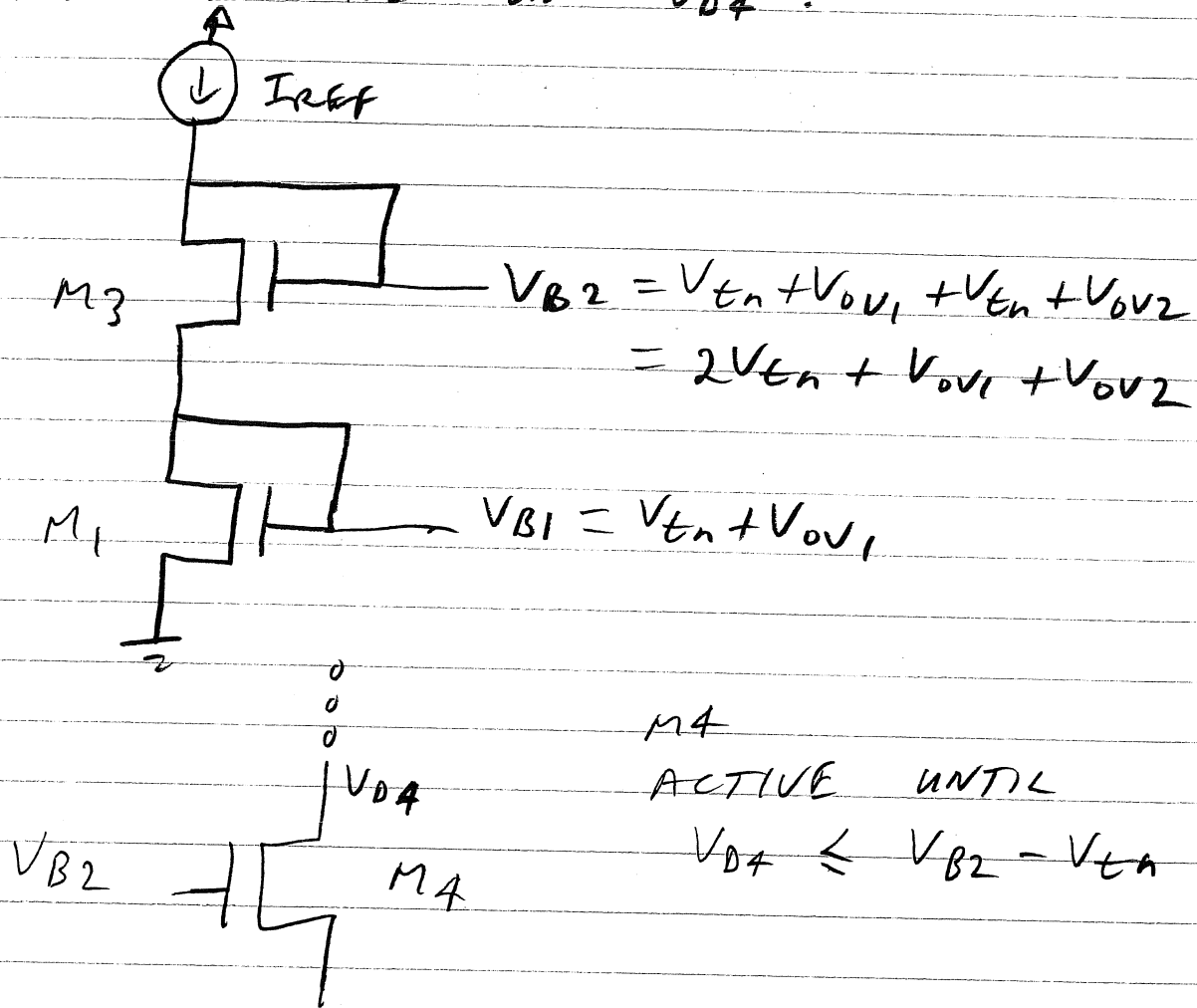
NORMALLY MATCH M1, M2 & M3, M4

=>  $L_2 = L_1$  &  $L_4 = L_3$

=>  $\frac{W_2}{W_1} = \frac{W_4}{W_3}$  SO THAT

$I_{out} = \frac{W_2}{W_1} I_{REF}$

MIN VOLTAGE ON  $V_{O4}$  ?



$$\begin{aligned} \text{MIN } V_{O4} &= 2V_{tn} + V_{ov1} + V_{ov2} - V_{tn} \\ &= V_{tn} + V_{ov1} + V_{ov2} \end{aligned}$$

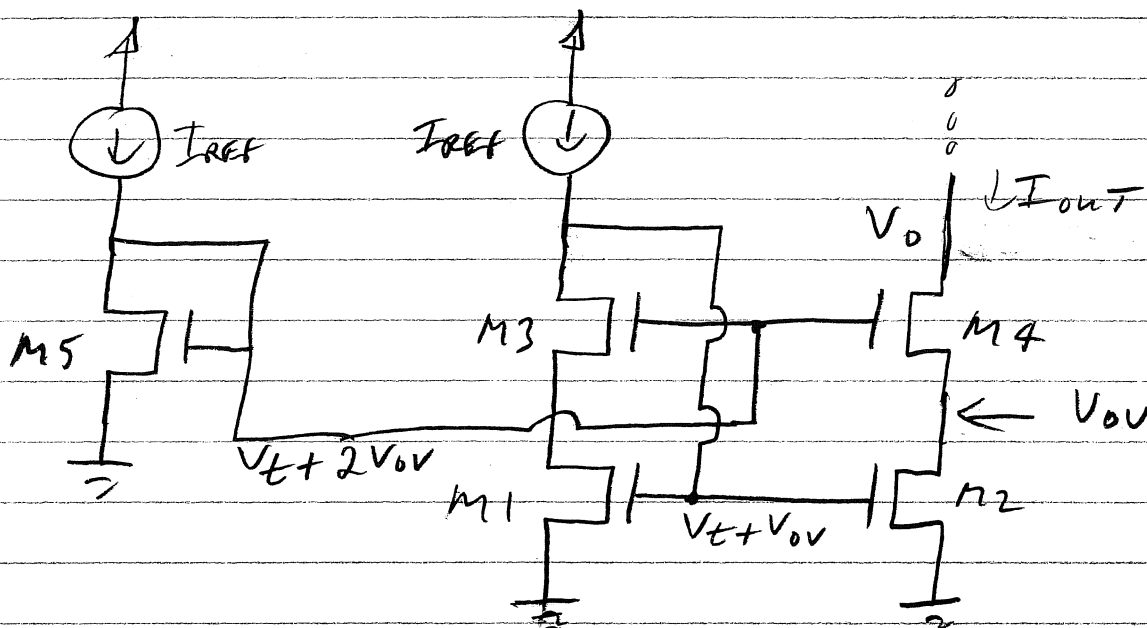
TYPICAL  $V_{tn} \approx 0.3V$   
 $V_{ov} \approx 0.2V$

SO MIN  $V_O \approx 0.7V$  NOT GREAT

WOULD LIKE TO LOWER  $V_{B2}$  SO  
M2 AT EDGE OF ACTIVE REGION

(CM8)

# WIDE SWING CURRENT MIRROR



ASSUME ALL  $\frac{W}{L}$  EQUAL FOR  $M_1 \rightarrow M_4$

BUT  $\left(\frac{W}{L}\right)_5 = \frac{1}{4} \left(\frac{W}{L}\right)_1$

DEFINE  $V_{ov} \equiv V_{ov1} = V_{ov2} = V_{ov3} = V_{ov4}$

CAN SHOW  $V_{ov5} = 2V_{ov}$

SO MIN  $V_o \approx 2V_{ov}$

(SINCE  $V_{G4} = V_t + 2V_{ov}$ )

GENERALLY  $\left(\frac{W}{L}\right)_5 \ll \frac{1}{4} \left(\frac{W}{L}\right)_1$  SO THAT

$M_2$  ENSURED IN ACTIVE